

High Performance Normally-Off Operation p-GaN Gate HEMT with Compositied Barriers Structure Design

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Abstract

In this work, a novel compositied barriers design of high electron mobility transistors (HEMTs) with normally-off operation mode composed of p-GaN/AlN/AlGa_{0.7}N/AlGa_{0.83}N/GaN structure was fabricated. Compared to the conventional p-GaN/AlGa_{0.83}N/GaN structure of HEMTs, the compositied barriers can effectively reduce the plasma-induced damage leading to the reduction of the increased dynamic ON-resistance (R_{ON}) after pulsed current-voltage stress operating. The excellent electrical characteristics of maximum drain current density and low subthreshold swing (S.S) of 320 mA/mm and 137 mV/dec, respectively, can be obtained in the proposed compositied barriers p-GaN gate structure of HEMT.

INTRODUCTION

In recent decades, GaN-based high electron mobility transistors (HEMTs) have attracted much attention in the high-voltage, high-power and device-switching applications due to their excellent material properties, such as high breakdown voltage, high switching frequency, low-channel resistance, and so forth. However, the normally-on operation characteristics of the conventional GaN-based HEMTs are usually not preferred in power electronic applications mainly due to their inconvenient operation and unavoidable power consumption. Thus, several researches have been proposed to realize the normally-off operation characteristics of the AlGa_{0.83}N/GaN HEMTs using various structures such as ultrathin barrier [1-2], gate-recessed HEMTs structures [3-4], triple cap layer and high-k gate dielectrics [5], deep-recess V-gate technology [6], and using a p-type capping layer [7] to reduce the concentration of two-dimensional electron gas (2DEG) in the channel of devices. However, the drain current density is much lower than normally-on devices, which results in the higher dynamic R_{ON} during device operation. Especially, these issues will be further degraded after electrical stress operating to cause the deterioration of device reliability. In the work, a novel compositied barriers structure using AlN capping layer in the p-GaN Gate HEMT with

normally-off operation is proposed to improve the drain current density and on-state resistance after the pulsed current-voltage (I-V) stress testing.

DEVICE STRUCTURE AND FABRICATION

Fig. 1 shows the schematic of the conventional and proposed structure with compositied barriers design in the p-GaN gate HEMTs. For the proposed p-GaN HEMTs, the epitaxial layers were grown on a Si (111) p-type substrate by metal organic chemical vapor deposition (MOCVD) which are composed of a 4 μ m-thick buffer layer, a 300 nm GaN channel, a 1nm Al_{0.3}Ga_{0.7}N barrier, a 12 nm Al_{0.17}Ga_{0.83}N barrier, a 1nm AlN capping layer and a 60 nm p-type GaN gate layer (Mg doping concentration = 3×10^{19} cm⁻³). The device fabrication started from defining the mesa area by reactive ion etching (RIE). The p-GaN island was formed by RIE with the etching gas BCl₃ + CF₄. Ohmic contacts was prepared by the electron beam evaporation to perform a multilayered Ti/Al/Ni/Au (25/120/25/150 nm) sequentially, followed by rapid thermal annealing (RTA) at 875 °C for 30 s in a nitrogen-rich ambient. After the gate region of Ni/Au (25/120 nm) metal layer was deposited by electron beam evaporator. Finally, a 200 nm-thick SiO₂ surface passivation layer was deposited via E-beam evaporator. The lengths of gate-to-source (L_{GS}), gate (L_G), gate-to drain (L_{GD}) are 2, 2 and 3 μ m, respectively. The width of device (W) is 50 μ m.

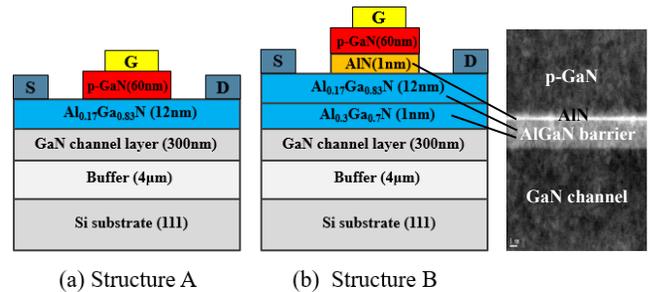


Fig. 1. Schematic structures of the p-GaN HEMTs with the (a) conventional barrier and (b) compositied barrier design.

RESULTS AND DISCUSSION

Fig. 2 shows the energy band diagram distributions of different structures. Compared with the conventional p-GaN HEMT, it clearly suggests the insertions of the wide band gap 1-nm AlN cap layer and the 1-nm $\text{Al}_{0.3}\text{Ga}_{0.7}\text{N}$ barrier in the proposed device can increase higher effective ΔE_C and polarization effect in the channel, respectively.

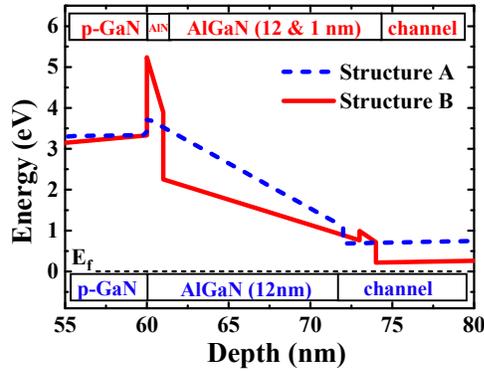


Fig. 2. The conduction band energy distributions of the structure A and B.

Fig. 3 displays the transfer characteristic conventional and proposed composited barrier structures at $V_{DS}=10$ V. It clearly suggests that the threshold voltage can be decreased from 2.1 to 1.7 V due to more 2DEG concentration in the channel caused by the increase of polarization effect caused by the insertion of 1-nm-thick $\text{Al}_{0.3}\text{Ga}_{0.7}\text{N}$ layer, described in Fig. 3. Furthermore, the off-state leakage can be improved by higher than one order of magnitude significantly in the proposed structure mainly due to the composited barriers of insertion of 1nm AlN capping layer. As a result, the proposed structure of HEMT shows an excellent S.S value of 167 mV/dec.

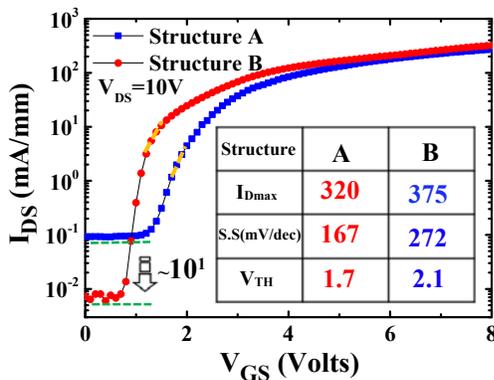


Fig. 3. The transfer characteristic of the structure A and B.

For the evaluation of current collapse behavior, the applied pulsed waveforms and timing diagrams are shown in Fig. 4. The device is switched from the off state with a V_{GSQ} of 0 V and V_{DSQ} is ranging from 0 to 200 V with a voltage step of 50V. The of V_{GS} and V_{DS} with pulse width of V_{GS} and period of V_{DS} are 2 μs and 200 μs . These transient OFF-to-ON switching I-V characteristics of the device is performed with an AMCAD pulsed I-V system.

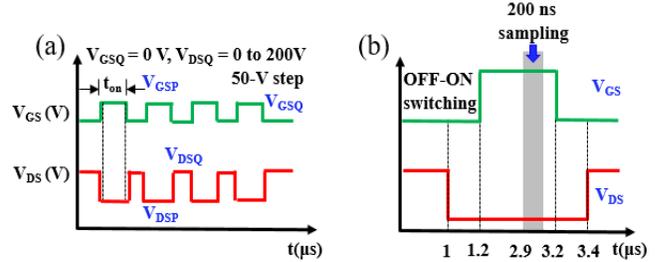


Fig. 4. Pulsed I-V characterization: (a) waveforms of V_{GS} and V_{DS} ; (b) timing diagrams of V_{GS} and V_{DS} with periods of OFF-to-ON switching (200 ns) and sampling time (200 ns) in ON-state.

Fig. 5 plots the DC and pulsed I_D - V_{DS} characteristics in the conventional and proposed structures of devices. The larger saturation current after stress is due to the field-assisted electron de-trapping from the traps at the drain-side gate edge. It clearly suggests the degradation of I_{DS} can be improved by approximately 10% in the structure B which implies the insertion of AlN capping layer can effectively reduce the generation of charge trapping states during the pulsed I-V stress periods.

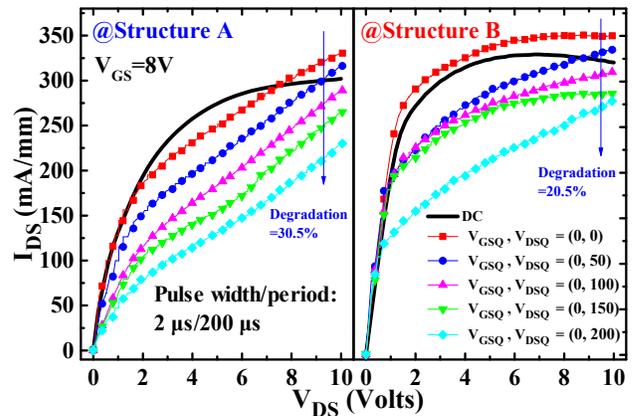


Fig. 5. Pulsed I_D - V_{DS} characteristics (with DC) were extracted from quiescent bias stress of (V_{GSQ} , V_{DSQ}) = (0 V, 0–200 V, step= 50 V) with pulse width/period of 2 μs /200 μs .

Fig. 6(a) shows dynamic on-state R_{ON} behaviors in the conventional and proposed structures of HEMTs after pulsed I-V stress. It is clear that the conventional structure of device severely suffers from the plasma damage induced current

collapse during pulsed I-V stress periods. Fig. 6(b) shows the dynamic on state current divided by static state current ratio. It reasonably suggests that the insertion of AlN capping layer can depress the generation plasma-induced damage leading to the decrease of the degradation of dynamic R_{ON} and dynamic on state current divided by static state current ratio during pulsed I-V stress.

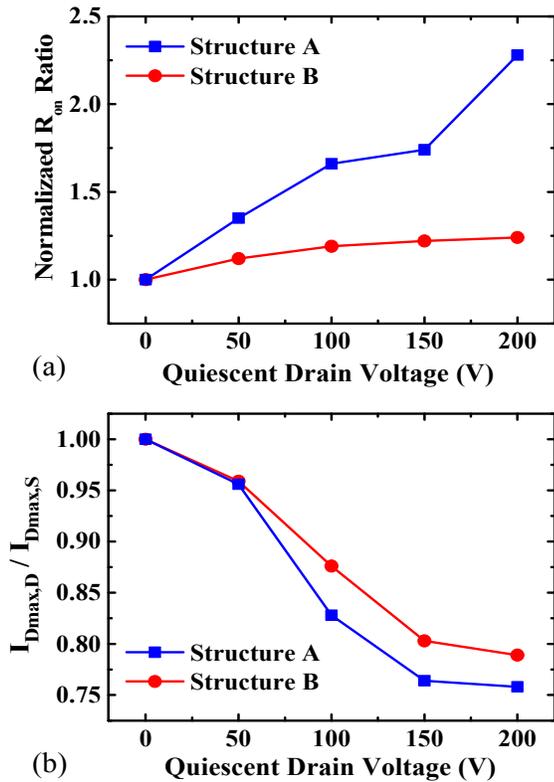


Fig. 6. With quiescent drain bias stress voltage of (a) Dynamic R_{ON} ratio and (b) $I_{Dmax,D} / I_{Dmax,S}$ ratio.

CONCLUSIONS

In this work, a novel structure of p-GaN HEMT was fabricated successfully. The decrease of threshold voltage suggests that the ability of gate control to channel is increased mainly due to more polarization effect induced more 2DEG concentration in the channel which is caused by the insertion of AlN capping and $Al_{0.3}Ga_{0.7}N$ layer. Additionally, the proposed HEMT significantly demonstrated that the plasma damage-induced in current collapse and dynamic on-state resistance can be improved by the composited barriers design using the insertion of AlN capping layer.

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ACRONYMS

HEMT: High Electron Mobility Transistor
2DEG: Two-Dimensional Electron Gas

