

Near Junction Thermal Transport and Embedded Cooling of High Power GaN Electronics

Carlton T. Creamer^{1*}, Pane C. Chao¹, Kenneth K. Chu¹, Adonis Kassinos¹, Geoffrey Campbell², Henry Eppich², A. Shooshtari³, S. Dessiatoun³, M. Ohadi³, Craig McGray⁴, Ray Kallaher⁴

¹Advanced RF Microelectronics, Technology Solutions, BAE Systems, Nashua NH

²Science Research Laboratories, Somerville, MA

³University of Maryland, College Park, MD

⁴Modern Microsystems, Silver Springs, MD

*e-mail: carlton.creamer@baesystems.com *Phone: 603-885-1275

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Abstract

Gallium-Nitride (GaN) MMIC circuits have been developed that achieve much greater RF power density compared to GaAs based predecessors. Even greater power densities are possible from these wideband gap devices. However, the requirement to maintain reliable junction temperatures limits both linear and areal power densities. Under the DARPA-sponsored NJTT and ICECool Applications programs, chip-scale thermal management solutions are being developed that combine GaN-on-Diamond with microchannel embedded cooling solutions that enable reliable MMIC operation at heat flux levels of $>1\text{kW}/\text{cm}^2$.

INTRODUCTION

Efforts to mature gallium nitride on silicon carbide (GaN-on-SiC) have been successful largely due to steady U.S. Government and industry investment for over a decade beginning around 2000 [1]. Although GaN-on-SiC devices now produce greater than 10x power density compared to the predominant predecessor GaAs [2], GaN has not yet been exploited to its full potential mostly owing to a limited ability to expel waste heat, and must therefore be operated at a derated electrical condition in order to maintain channel temperatures at or below levels required for 10^6 hours of reliable operation. With Near Junction Thermal Transport and Embedded Cooling of High Power GaN Electronics, thermal limitations are overcome through the use of embedded, chip-scale thermal management techniques that are the critical enablers to achieving increased power density, leading to a significant system performance advantage. Chip-scale thermal management combines the use of a passive diamond MMIC substrate that replaces the native SiC via a bonding method [3] with a high performance microchannel cooler that boasts volumetric heat capacity of greater than $10\text{kW}/\text{cm}^3$ [4].

MOTIVATION AND PERSPECTIVE

1) Higher RF power density provides flexibility to the system designer to conduct performance trades of range, cooling, SWaP, reliability, and payload capability/volume. For example, greater power per element will produce AESAs with increased effective range for electronic attack or radar. Alternatively, the array may be configured with fewer higher power elements in a “sparse array” in order to lower size and weight or cost. This in turn enables low volume payloads for deployment on small platforms.

TABLE I
SYSTEM FLEXIBILITY ENABLED BY
CHIP-SCALE THERMAL MANAGEMENT



	GaN-on-SiC	GaN-on-Diamond			
		High Reliability	High Power per Element	Relaxed Baseplate Temp.	Very High Power
Performance		• Same performance, higher reliability (MTTF)	• Higher power • Same reliability (MTTF)	• Equivalent reliability (MTTF) and performance • Operate at higher baseplate temperatures	• High power, short lifetime • Not thermally limited
System Impact		• Greater Mission Lifetime	• Greater range and capability • Reduced element count	• Reduced cooling Slew • Enables payloads on smaller platforms	• Very High power in small volumes
Channel Temp.					
Baseplate Temp.					
RF Power					

2) Reduced Cooling System Size and Power-Typically, a coolant pumping system can consume ~20% of the overall system’s available prime power. Modern, large phased array systems require liquid cooling to maintain chassis baseplate temperatures at small deltas above fluid inlet. Through the application of embedded cooling technology, the total thermal resistance to the semiconductor junction can be lowered, allowing for a relaxation in the baseplate temperature requirement. Using embedded cooling, a 25°C

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relaxation is possible which translates to a >2X reduction of coolant pumping power (which approximately equates to a similar size and weight reduction) for a PAO cooled, 60kW load [5].

3) System Reliability- Solid state transmitter reliability is dominated by power amplifier junction temperature. A 10°C reduction in junction temperature results in approximately 5X improvement in device lifetime for a typical GaN process (reliability $E_A \sim 2eV$). This can significantly lower transmitter life-cycle cost and extend mission lifetimes.

CHIP-SCALE EMBEDDED COOLING

Typical GaN-on-SiC MMIC amplifiers are configured in CTE matched metal packages that rely on conduction cooling. In these configurations, the majority of the temperature rise occurs within the MMIC chip boundary (Figure 1). Attempts at lowering junction temperature by modifying the external packaging in the remote cooling regime will be only marginally effective. Significant thermal enhancements must be targeted near the device junction and within the embedded cooling zone.

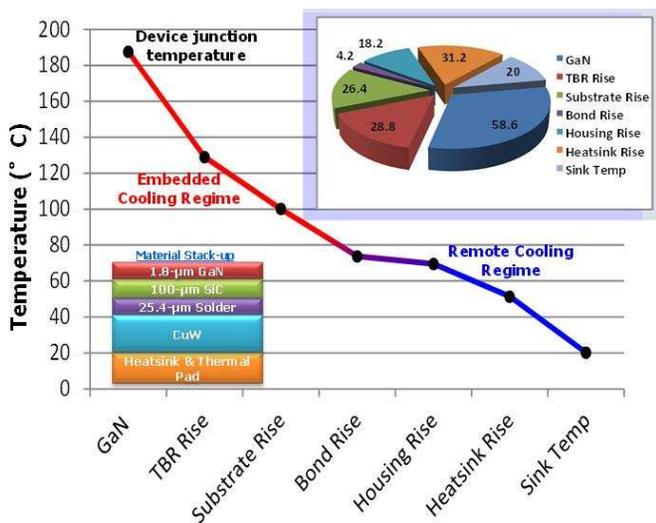


Figure 1- Temperature rise in a typical GaN-on-SiC amplifier construct

GaN-ON- DIAMOND

GaN-on-Diamond transistors fabricated under the DARPA Near Junction Thermal Transport Program (NJTT) [6],[7] have been demonstrated with RF output power levels as high as 11W/mm at 10GHz. Transistor level areal power densities of >3.5X compared to GaN-on-SiC have been achieved. Figure 2 shows IR images of a typical GaN-on-SiC 4x50µm transistor and (left) and a 12x50µm GaN-on-Diamond transistor (right) with three (3) times the number of gate fingers in the same mesa area, creating a 3X increase

in power density. The images show peak temperatures for the GaN-on-Diamond transistor that are 7°C lower exemplifying the low thermal boundary resistance at the GaN to diamond interface and the excellent lateral and through-plane thermal conductivity of the CVD polycrystalline diamond substrate.

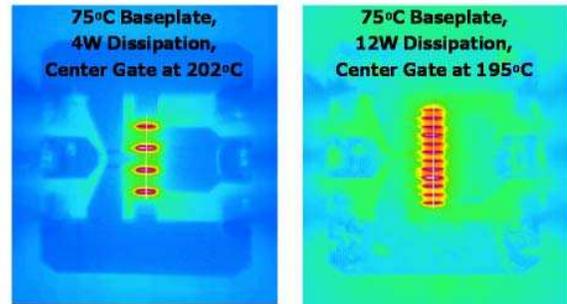


Figure 2-IR image of GaN-on-SiC (Left) and GaN-on-Diamond (Right) Transistors

GaN-on-Diamond MMIC circuits are currently in development under the DARPA ICECool Applications Program [8,9]. Simulations show 12W avg. RF power from 2-18GHz in a footprint <2.85mm². These circuits have waste heat densities of >1kW/cm² while maintaining junction temperatures below 240°C. Figure 3 is an optical image of a fabricated 2-18GHz MMIC amplifier.

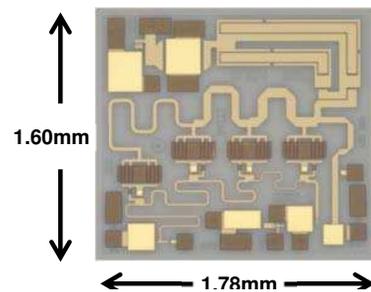


Figure 3- Optical image of GaN-on-Diamond MMIC (in fabrication)

SINGLE PHASE MICRO-CHANNEL COOLER

GaN-on-Diamond MMIC circuits are mounted onto a single phase microchannel cooler that uses a 50/50 EGW working fluid (Figure 4). The cooler is fabricated by bonding a series of half-etched metal foils that are patterned to achieve the desired micro-channel geometry. Solid metal is easily added at the cooler boundaries during the fabrication process to extend the plane that forms the RF ground required for

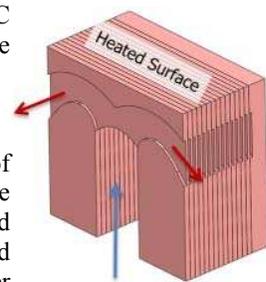


Figure 4-Single Phase Micro-channel Cooler

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ancillary circuitry within the multi-chip module (MCM).

The design was optimized by parameterizing the 3D cooler geometry as a series of arcs and linear segments to support analysis using a multi-objective optimization method. The targeted performance objectives included minimal thermal resistance and pressure drop, while constraining peak flow velocity below limits established by erosion models. Simulation results for a heat flux = 1000 W/cm² and areal flow rate = 2.84 L/min-cm² showed thermal resistance of $R_{\text{Thermal}} = 22.4 \text{ K-cm}^2/\text{kW}$ measured between the fluid inlet and the heated surface and a $\Delta P = 17.6 \text{ psi}$. Cooler performance was tested by measuring the temperature of a thin film TaN resistor using an IR camera to determine peak temperature, then calculating the cooler thermal resistance. Pressure drop was measured using the built-in pressure sensor at fluid I/O. Using standard lithography, a 16.6Ω resistor was fabricated on a 2.65mm x 2.65 mm x 0.15mm polycrystalline diamond substrate to closely approximate the MMIC size and was configured as six (6) parallel 100Ω, 100μm x 400μm thin film resistors that allowed for selective wiring and created a “Hot Spot”. Tests were performed at a fluid inlet temperature of 22 °C with a measured flow rate of 3.13 L/min-cm². Power supply voltage of 34.9V was applied. Measured current was 2.10A for a total dissipation of 73.4W. The IR image test result is shown in Figure 5. The measured peak temperature of 50 °C is consistent with simulated results of CFD modeling of the DUT. Measured heat flux of the chip surface was 1046W/cm² while hot spot heat flux of the 100μm x 400μm resistor was 30.7kW/cm².



Figure 5-IR temperature measurement of GaN-on-Diamond resistor mounted to micro-channel cooler

THERMAL DEMONSTRATION VEHICLE (TDV MMIC)

The effectiveness of the complete embedded cooling solution will be tested by constructing a Thermal Demonstration Vehicle (TDV). The TDV assembly will combine the GaN-on-Diamond MMIC with the high heat capacity micro-channel cooler that is embedded into the RF ground plane. (see Figure 6). The electrical components,

including the MMIC, RF and DC substrates, and bias injection circuits are assembled onto the top side of the cooler using conventional assembly processes similar to an ordinary MCM. The bottom surface of the TDV serves as the interface to the fluid I/O and SMA connections to the RF source and load which are positioned orthogonally.

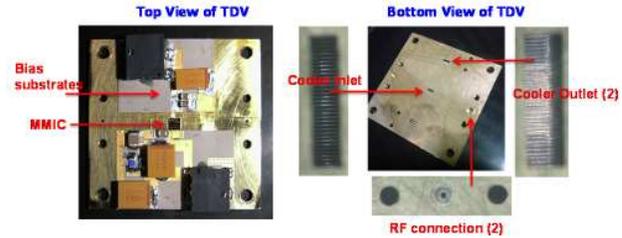


Figure 6-Single phase micro-channel cooler

CONCLUSIONS

System designers will always push to add functionality or performance enhancements that will increase electronics density within fixed payload volumes. The resulting increase in waste heat density will tax conventional thermal management approaches beyond current capability to handle the projected extreme heat loads. Advancements in embedded thermal management like diamond substrate materials and microcooler packaging are important enabling technologies that will allow systems designers to realize higher performance transmitters in smaller available envelopes.

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ACRONYMS

NJTT: Near Junction Thermal Transport
ICECool: Intra-Chip Enhanced Cooling
MMIC: Microwave Monolithic Integrated Circuit
SWaP: Size, Weight and Power
AESA: Active Electronically Steered Array
PAO: Polyalphaolefin
CTE: Coefficient of Thermal Expansion
EGW: Ethylene Glycol and water
CVD: Chemical Vapor Deposition
CFD: Computational Fluid Dynamic

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